

Power Factor Correction in a Distribution System: An Optimization Approach

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Abstract- This paper presents an efficient algorithm to solve the radial distribution power flow problem in complex mode. The relationship between the complex branch powers and complex bus powers is derived as a non singular square matrix known as element incidence matrix. The power flow equations are rewritten in terms of a new variable as linear recursive equations. The linear equations are solved to determine the bus voltages and branch currents in terms of new variable as complex numbers. The advantage of this algorithm is that it does not need any initial value and easier to develop the code since all the equations are expressed in matrix format. It is tested on the distribution systems available in the literature. This proposed method could be applied to distribution systems having voltage-controlled buses also. The results prove the efficiency of the proposed method. In this paper a new method is proposed to improve the power factor of the buses having low power factor.

Keywords- Dimension reducing distribution load flow algorithm, Electrical Distribution Network, Power factor.

I. INTRODUCTION

The distribution systems are characterized by their prevailing radial nature and high R/X ratio. This renders the load flow problem ill conditioned. So many methods [1-8] have been developed and tested ranging from sweep methods, to conic programming formulation. Early research indicated that standard load flow methods fail to converge for ill-conditioned test systems [9]. The basis for the all the sweep methods is that they need an initial value (normally flat) for the voltages and the updating is done in forward and backward way implementing the kirchoff's equations. Expósito and Ramos [8] have proposed a radial load flow technique based on solving a system of equations in terms of new variables and using the Newton approach. Conic programming formulation is [9] to model the power flow problem as a conic optimization problem in terms of new variables. Both the methods the number of variables to be determined is $3N$ for an N bus radial system. This paper exploits the radial structure of the distribution network and the relationship between the bus powers and branch powers is expressed as a non-singular square matrix known as element incidence matrix.

The paper is organized into four sections. The first section describes the conventional radial distribution power flow problem, the second section derives the proposed method for PQ buses, third section deals with treatment of voltage-controlled buses and the fourth section discusses the simulation results. Radial systems of 12, In [10] the power factor of the buses having low power factor is not improved.

II. DISTRIBUTION POWER FLOW

The distribution power flow is different from the transmission power flow due to the radial structures and high R/X ratio of transmission line. Because of this conventional transmission power flow algorithms does not converge for distribution systems. In this dimension reducing power flow [11] is implemented to determine the power factor and to improve the power factor of the buses of low power factor. The distribution power flow algorithm is the heart of this method.

A. Dimension reducing load Flow Algorithm

The basis for the proposed method is that an n -bus radial distribution network has only $n - 1$ lines (elements) and the branch currents (powers) can be expressed in terms of bus currents (powers). For an element ' ij ' connected between nodes ' i ' and ' j ' the bus current of node j can be expressed as a linear equation. In terms of branch current.



$$I_j = I_{ij} - \sum_{k(j)} I_{j,k(j)} \quad (1.1)$$

$k(j)$ is the set of nodes connected to node j . For the slack bus the power is not specified, so it is excluded and the relationship between remaining bus currents and branch currents are derived as a non-singular square matrix.

$$I_{bus} = K X I_{branch} \quad (1.2)$$

$$I_{bus} = [I_{b2}, I_{b3} \dots I_{bn}] \quad (1.3)$$

The matrix K is named element incidence matrix. It is a non-singular square matrix of order $(n - 1)$. I_{bus} is the column matrix of size $n-1$. The elemental incidence matrix is constructed in a simple way same like bus incidence matrix. In this matrix K each row is describing the element incidences. The elements are numbered in conventional way i.e. the number. of element ' j ' is $(j - 1)$.

- The diagonal elements of matrix K are one. The variable j is denoting the element number.

$$K(i, j) = 1 \quad (1.4)$$

- For each ' j ' the element let $m(j)$ is the set of element numbers connected at its receiving end.

$$K(i, m(j)) = -1 \quad (1.5)$$

- All the remaining elements are zero. It can be observed that all the elements of matrix K below the main diagonal are zero.

$$I_{branch} = K^{-1} X I_{bus} \quad (1.6)$$

The relationship between the branch currents and bus currents can be extended to complex branch powers and bus powers. The sending end power and the receiving end powers are not same due to transmission loss. The transmission loss is included as the difference between the sending end/receiving end powers derived. The relationship between branch powers and bus powers is established in same way of bus/branch currents. Multiplying both sides by element incidence matrix K .

$$S_{bus} = K[S_{branch}^{sending} - TL_{branch}] \quad (1.7)$$

$$S_{branch} = K^{-1}S_{bus} + TL_{branch} \quad (1.8)$$

The power flow equations are complex multi variable quadratic equations. A new variable R_{ij} is introduced for each element ' ij ' and the equations becomes recursively linear.

$$R_{ij} = V_i(V_i^* - V_j^*) \quad (1.9)$$

The branch power of ' ij ' th element is expressed in terms of R_{ij}

$$S_{ij} = P_{ij} + jQ_{ij} = R_{ij}Y_{ij}^* \quad (1.10)$$

$$R_{ij} = S_{ij}Z_{ij}^* \quad (1.11)$$

The dimension reducing power flow method is summarized as following steps.

Step 1: For the first iteration transmission losses are initialized as zero for each element.

From the bus powers specified the branch powers are determined as per equation (1.7 & 1.8).

Step 2: The variable R_{ij} is determined for each element using equation (1.9).

The bus voltage, branch current and bus current are determined from R_{ij} .

$$V_j = V_i - \left(\frac{R_{ij}}{V_i} \right)^* \quad (1.12)$$

$$I_{ij} = \left(\frac{R_{ij}}{V_{ij}} \right)^* Y_{ij} \quad (1.13)$$

Step 3: The bus currents are determined from (1.1) and bus powers are calculated. Since the transmission losses are neglected in the first iteration there will be mismatch between the specified powers and calculated powers. The mismatch is a part of the transmission loss. TL_{ij}^r is the transmission loss part for ' ij 'th element for ' r 'th iteration. Transmission loss of each element is the summation of the transmission loss portions of all previous iterations.

$$TL_{ij} = \sum_1^r TL_{ij}^r \quad (1.14)$$

Where r is the iteration count

$$TL_{ij}^r = K^{-1} \left(S_j^{spec} - V_j^{r-1} I_j^* \right) \quad (1.15)$$

$$S_{ji} = S_{ij} - TL_{ij} \quad (1.16)$$

$$S_{branch}^{sending} = S_{branch}^{receiving} - TL_{ij} \quad (1.17)$$

It can be concluded that the power flow solution always exists for a distribution system irrespective of the R/X ratio if it is having connectivity from the source (slack bus) to all the nodes. For system having less transmission loss the algorithm will perform faster. The convergence criteria is that during the ' r 'th iteration the mismatch of power should be less than the tolerance value.

B. Distribution load flow Software Development

After studying and rewriting the power flow equations, a new solution methodology has been developed to determine the voltage profile and power losses in radial distribution system.

The algorithm for Distribution Power Flow summarized as follow.

Step 1: Assume base MVA, base KV, slack bus voltage, and initial transmission losses

Step 2: Read the data.

Step 3: Form the bus incidence matrix K .

Step 4: Determine the inverse of bus incidence matrix K .

Step 5: Form the complex power matrix ' S ' for the remaining buses (from 2 to n) from the data.

- Step 6:** Store the specified bus powers in a new matrix $S_{spec} = S$.
- Step 7:** Find out the branch power using the equation (1.8).
- Step 8:** Determine the impedance matrix from the data and express in a per unit impedance matrix.
- Step 9:** Find out nodal voltage at each nodes using the equation (1.12).
- Step 10:** Find out the branch and bus currents for the network using the equations (1.2 to 1.16).
- Step 11:** Find out the calculated bus power for all nodes. (1.7)
- Step 12:** Find out the transmission losses using equation (1.17) and add it to specified bus and repeat for 'r' iterations till convergence.

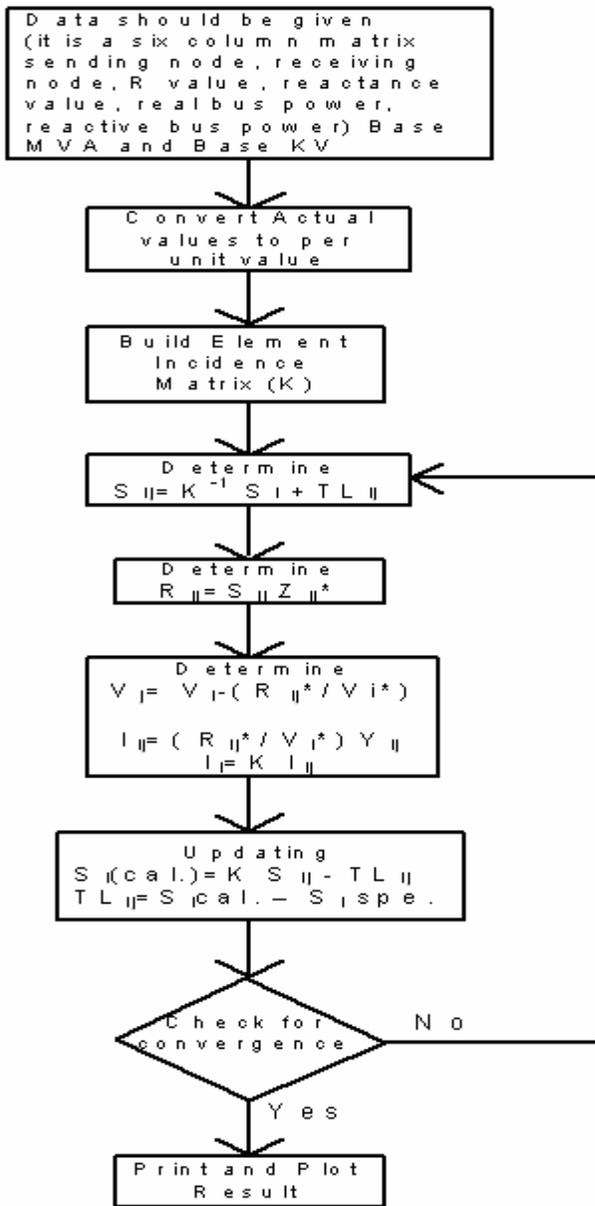


Fig. 1: Flow chart for DRD load flow

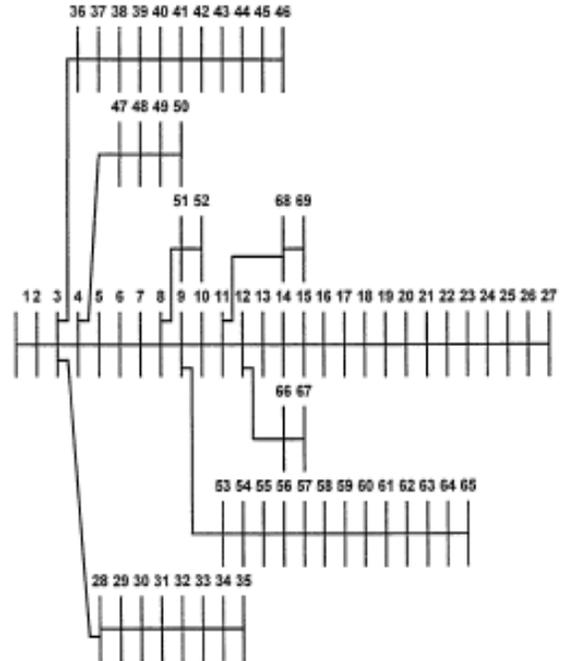


Fig. 2: IEEE 69 bus system

In this the power factor of all the 69 buses is determined, after that the buses having low power factor is found out and then the power factor of the buses having low power factor is set to unity and then by running the load flow is conducted.

Energy Rate = \$4.08 per KWH
Demand Charge = \$2.16 per KW
PF Penalty = \$0.15 per KVARH

TABLE 1: POWER FACTOR CORRECTION

Bus No	Original Power factor	Corrected Power factor	KVAR required
5	0.7633	1	2.2
9	0.7791	1	3.5
40	0.768	1	1
Total KVAR required			6.7

TABLE 2: SAVINGS AT BUS 5 DUE TO PF CORRECTION

Bus No	5
Savings in Energy usage in \$/month	161.575
Saving in demand charge	0.11717

in \$/month	
Savings due to power factor penalty in \$/month	240.9

TABLE 3: SAVINGS AT BUS 9 DUE TO PF CORRECTION

Bus No	9
Savings in Energy usage in \$/month	254.563
Saving in demand charge in \$/month	0.18461
Savings due to power factor penalty in \$/month	383.25

TABLE 4: SAVINGS AT BUS 40 DUE TO PF CORRECTION

Bus No	40
Savings in Energy usage in \$/month	73.268
Saving in demand charge in \$/month	0.05313
Savings due to power factor penalty in \$/month	109.5

TABLE 5: ANNUAL SAVINGS DUE TO PF CORRECTION

Saving/Cost	With power factor correction
Savings at Bus No 5 in \$/month	402.59
Savings at Bus No 9 in \$/month	637.99
Savings at Bus No 40 in \$/month	182.82
Total cost of capacitor in \$	20.1
Total Savings/month in \$	1203
Total Savings/year in \$	14,436

III. CONCLUSION:

This study presents DRD load flow method to solve the IEEE 69 Bus Problem regarding power factor correction in the distribution system. Using this method Energy savings, savings in demand and savings in power factor penalty are obtained.

As the KVAR required is small to correct the power factor, cost of the capacitor required for power factor correction is also very less. By using this method the overall system performance can also be improved. Because of the improvement in the power factor at the buses having low power factor the voltage profile of the system also improves. Finally this method is useful for the consumers who requires the power factor nearer to unity.

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